
Overwash hazard assessment

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| A B S T R A C T |

Overwash is a natural storm-related process that occurs when wave runup overcomes the dune crest. Because coastlines are globally occupied, overwash is a hazardous process and there is a need to identify vulnerable areas. This study proposes a method to detect overwash-prone areas in the Ancão peninsula, Portugal, and eventually outlines a vulnerability map. Dune base (D_{LOW}) and crest (D_{HIGH}) topography were surveyed. Three different storm scenarios (5-, 10- and 25- year return period storms) and associated waves and sea level were determined. According to these data, extreme wave runup (R_{HIGH}) was calculated by a parameterisation set for intermediate-reflective beaches. The maps for collision and overwash regimes were designed by comparing R_{HIGH} values with D_{LOW} and D_{HIGH} . Almost the entire dune base along the peninsula is vulnerable to collision regime. The overwash process was identified mainly along the tidal inlet hazard area and within the human-occupied portion of the beach, where overwash is expected to occur within 5 years of return period. The developed method considers the main overwash driving forces and proved to identify hazardous areas previously observed in the area. Occasional differences between modelled and observed overwash areas can be attributable to equipment errors, morphology interpretation subjectivity and maladjustments in runup parameterisation. Nevertheless, the method proved to be effective in reproducing the overall Ancão peninsula vulnerability and can be widely applied. Therefore, it is a simple and potentially important tool for coastal management that enables mitigation strategies for occupied coasts and assessment of geological and ecological consequences in natural areas.

KEYWORDS | Overwash. Storm Surge. Runup. Barrier Island. GIS.

INTRODUCTION

In the present scenario of intense development along the world's coastlines, storm impact is one of the hazards responsible for coastal vulnerability. Overwash is one of the most dramatic consequences of storms on barrier islands, at pristine or developed sandy coasts with dunes and thus responsible for a substantial part of the hazard. In conditions of high wave runup (swash elevation superimposed on storm surge and tidal levels and wave setup)

the level reached by the water is competent to overpass the beach crest (or coastal defence), originating overwash (or overtopping) flow. Overwash occurs throughout a singular combination of oceanographic and foreshore geomorphologic factors. Some of the morphologic factors driving overwash are: nearshore bathymetry (*e.g.*, Ritchie and Penland, 1988), beach topography (*e.g.*, Matias *et al.*, 2009), and backbeach elevations (*e.g.*, Morton and Sallenger, 2003). Sallenger (2000) defined storm impacts including overwash and collision regime (erosion induced by runup

reaching the dune base). Because an overwash event is an important natural sedimentation-erosion process (Leatherman, 1979) that promotes significant changes to coastal systems there is a demand to predict their occurrence and to define the vulnerability of a coastal area to such events.

Vulnerability and hazard concepts are stated in Ferreira *et al.* (2009). Vulnerability is considered as a function of the hazard represented by forcing conditions (wind, waves and tidal levels) that favour damage, and the predisposition of people and properties to be affected by marine storms. When referring to a geomorphic component, vulnerability accounts for the modification of the coastal substrate (*e.g.*, morphodynamic response to storms) (Jiménez *et al.*, 2009). Hazard is the probability of a given danger (threat) to occur within a given period (Ferreira *et al.*, 2009) and therefore represents a level of threat to life, health, property or environment. The two fundamental components of any natural hazard are magnitude and frequency (with an assumption that the higher the magnitude, the lower the frequency) (Doornkamp, 1998). According to Jiménez *et al.* (2009) the magnitude of coastal response to storms depends on both the magnitude of the forcing (storm properties) and the receptor characteristics (coastal geomorphology). Consequently, in order to assess overwash and collision regimes vulnerability is necessary to define potential storm conditions (represented by runup levels) and coastal morphology which may be affected (comprised by dune base and crest elevations) by such energetic conditions.

The aim of this paper is the development and application of overwash hazard assessment tools that translate into the establishment of areas vulnerable to storm erosion and overwash. The developed methodology is applied to the Ancão peninsula, in the southern coast of Portugal. Vulnerability maps are eventually designed and advised as valid tools for coastal zone management and decision making.

STUDY AREA

The study area is the Ancão peninsula, which is located on the Ria Formosa barrier island system, a physiographic unit in southern Portugal (Fig. 1). The system displays a cusped shape with western and eastern flanks, NW-SE and NE-SW oriented, respectively. The Ancão peninsula is located on the western flank of the barrier island system. The study area is mesotidal with a mean tidal range of 2.8m during spring tides and of 1.3m during neap tides with a maximum tidal range of 3.5m. According to Costa (2001), the offshore wave climate is dominated by W-SW waves (71% of occurrences) and southeast waves (short period waves, generated by winds locally designated as Levante) are also frequent (about 23%). Wave energy is moderate with a significant annual average offshore height of

1.0m and an average peak period of 8.2s. Significant wave height lower than 1m is registered during 68% of the year. A storm is defined as an event with significant offshore wave height higher than 3m (Pessanha and Pires, 1981; Melo, 1989; Costa, 1994). Southwest storm waves have a significant average height which is higher than Levante storms (Costa, 1994). Southwest storms account for 64% of occurrences and southeasterly storms for 32%. A 5m SE storm has an estimated return period of 50 years, whereas a 5.7m SW storm is expected to occur every 5 years (Pires, 1998). The Ancão peninsula is directly exposed to W-SW waves, and relatively protected from Levante waves.

The length of the Ancão peninsula is variable (from 8.5 to 12.8km between 1947 and 2001; Matias *et al.*, 2008) due to changes in the position of the Ancão Inlet, which migrates eastward at rates of 40 to 100m/year (Vila-Concejo *et al.*, 2006). The peninsula is narrow, ranging from 50 to 250m in width, with dunes that can be single crested and reach 5.5m above mean sea level (Matias *et al.*, 2008).

The eastern part is a low-density population area, consisting of a fishing village located mainly in the back-barrier margin. It is a dynamic area and the ocean front evidences accretion by the existence of a wide and vegetated backshore. Dunes are lower and incipient and periodically overwashed (Ferreira *et al.*, 2006). The central area of Ancão peninsula includes Praia de Faro, where the construction of recreational and residential infrastructure is responsible for dune ridge lowering and destruction. Some parts of the ocean front have been artificially stabilised with revetments in order to avoid shoreline retreat. These structures inhibit shoreline retreat but are often overwashed both during storm (Ferreira *et al.*, 2006) and non-storm conditions, as previously observed in equinoc-

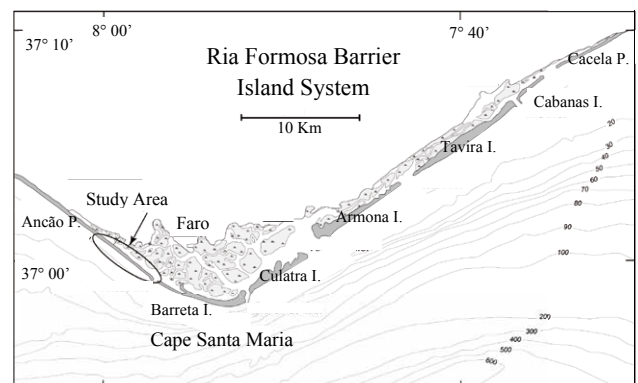


FIGURE 1 | Location of the Ria Formosa barrier island system, comprising tidal inlets (in italics), I: islands, P: peninsulas and mainland cities. The area encircled represents the study area (adapted from Matias *et al.*, 2009).

tial spring tides (Matias *et al.*, 2008). The western area is characterised by a stable and continuous foredune with blowouts and bluffs. There is a permanent scarp defining an ongoing shoreline retreat process (Ferreira *et al.*, 2006).

METHODS

Topographic data

Topographic measurements were made using a RTK-GPS, recording at 1Hz. Two types of surveys were undertaken: cross-shore profiles (October 2008) and alongshore alignments (November 2008). Sixteen profiles across the barrier island were surveyed every 300m covering a total extent of approximately 5km. Alongshore surveillance measured the dune base and crest. The dune crest was set as the highest portion of the frontal dune, *i.e.* where sand was mainly driven by aeolian processes and well developed dune vegetation could be observed. Where the dune crest was not present, *e.g.* along an urbanised area, it was defined as the top of the frontal construction line (generally walls). The dune base was considered the lowest part of the foredune (foreshore limit) or the base of the frontal construction along the urbanised area.

For a detailed analysis of barrier alongshore variability ten sectors were defined along the study area. The criteria for such individualisation were foreshore morphology, dune elevation and human occupation. The mean beach face slope was computed for each defined coastal sector, from the berm crest to approximately 1m below mean sea level.

Hydrodynamic data

Wave, tide and storm surge data from June 1997 to June 2007 were used for this study. Offshore wave data were recorded by Instituto Hidrográfico de Portugal with a directional wave-rider buoy off Santa Maria cape (Fig. 1) at 93m depth (Costa, 1994). Records were obtained for 20min every 3h, except during storm periods when data was recorded every half an hour. Storm events were identified for the 10-year period. Because W-SW storms are dominant and more energetic and the study area is relatively protected from E-SE waves, only western quadrant waves ($180^\circ < \theta < 270^\circ$) were accounted. Eventually, storm wave data were reduced to the highest daily record of significant wave height and associated parameters.

According to the Instituto Hidrográfico de Portugal (1998), Faro's coast has mean spring and neap high-tides of 1.4m and 0.64m above mean sea level, respectively. The average (*i.e.*, mean high water level that is exceeded by 50% of high tides) rises 1m above mean sea level. The

latter was considered for the present analysis as the tidal phase over which each storm occurs.

Because of the absence of measured water levels at the study area, surge levels were compiled by the REDMAR database, a tide gauge network from the Spanish Port System (Puertos del Estado, 2009). Data were gathered from a tide gauge located at the port of Huelva, Spain (80km from the study area). Storm wave data, previously identified, were linked to the equivalent highest daily storm surge registered by REDMAR to determine surge levels associated to storm events.

Assessment of overwash and collision hazard

The determination of overwash and collision hazards was based on a storm impact scale proposed by Sallenger (2000). The approach is based on the elevation of R_{HIGH} relative to the elevation of critical geomorphic features on barrier islands. Critical features along barrier islands are dune base and dune crest, defined as D_{LOW} and D_{HIGH} , respectively. By considering how R_{HIGH} varies relative to D_{HIGH} and D_{LOW} (Fig. 2), a series of storm impacts can be defined. Along beaches where there is a foredune ridge, as R_{HIGH} increases runup will eventually collide with the base of the dune, inducing erosion. The collision regime occurs when R_{HIGH}/D_{HIGH} exceeds D_{LOW}/D_{HIGH} . As R_{HIGH} continues to increase, overwash of a dune crest occurs when $R_{HIGH} > D_{HIGH}$.

In order to predict overwash hazard during a storm occurrence, three scenarios with different return periods were defined: 5, 10 and 25 years. For each of these return periods, the highest elevation of runup (R_{HIGH}) was calculated (equation 1), according to Sallenger (2000):

$$R_{HIGH} = R_2 + \eta_{mean} \quad (1)$$

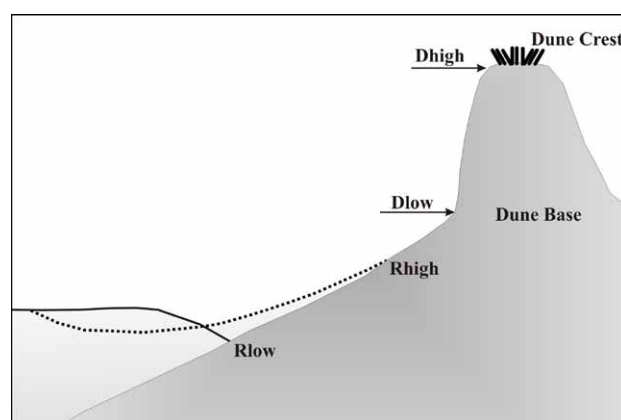


FIGURE 2 | Sketch describing variables used in scaling the impact of storms on barrier islands (adapted from Sallenger, 2000).

where R_2 is the runup that has exceeded 2% of the registered time and η_{mean} is mean sea level (the sum of the astronomical tide and the storm surge). R_2 was obtained through the empirical parameterisation given by Stockdon *et al.* (2006):

$$R_2 = 1.1 \left(0.35 \beta_f (H_S L)^{\frac{1}{2}} + \frac{[H_S L (0.563 \beta_f^2 + 0.004)]^{\frac{1}{2}}}{2} \right) \quad (2)$$

where β_f is the foreshore slope, H_S is the significant wave height and L is the wavelength, defined as $gT^2/2\pi$. Equation (2) is parameterised according to the wave-induced setup ($0.35 \beta_f (H_S L)^{1/2}$), and the swash, both incident ($0.563 \beta_f^2$) and infragravity (0.004) and it should be applied to the intermediate-reflective range of beach conditions (Stockdon *et al.*, 2006).

Significant wave height and associated θ corresponding to a 5-, 10- and 25-year return period event were ascertained by Pires (1998) using measured data. A linear trend was derived from the plot of H_S and T_p for the entire period of analysis and used to interpolate T_p for three storm scenarios. To determine standard values of storm surge (S) for the three given storms, a linear relation between the highest H_S and associated S was derived.

The elevation values obtained for R_{HIGH} were compared to dune base and dune crest topography. In order to assess the vulnerability to collision and overwash regimes, a map was designed setting the topographic layers relative to the dune base (D_{LOW}) and crest (D_{HIGH}) and comparing them to previously calculated R_{HIGH} values. For any given point where the dune base/crest topography was lower than the calculated storm-induced runup, the area was categorised as vulnerable to collision/overwash. Using Geographic Information System (GIS) the vulnerable areas were represented as buffers with different colours in order to differentiate the vulnerability relative to the three storm scenarios.

RESULTS

The ten individualised sectors are represented in Figure 3. The lowest dune elevation is in the easternmost segment of the beach (Sector 1, Table 1), whereas the highest elevation is located westward (Sector 10, Table 1). Beach steepness varies within this morphologic sketch, becoming more reflective westward.

Significant wave height (H_S) and associated peak period (T_p), as well as significant wave height (H_S) and associated storm surge (S) for stormy waves show evident but not significant positive correlations for a p-value less than 0.05 (Fig. 4). The linear trend for $H_S \times T_p$ (Fig. 4A) is represented by the equation $y = 0.834x + 6.565$. The plot $H_S \times S$ (Fig. 4B) shows a linear relation given by $y = 0.111x - 0.175$. The existence of these trends allowed the calculation of T_p and S associated to H_S of 5, 10 and 25 years of return period determined by Pires (1998; Table 2). The determined S values were added to the mean high water level (1m), considered as the base level over which the storms act. These hydrodynamic parameters were used to compute R_{HIGH} (equations 1 and 2) and were combined with dune parameters (D_{LOW} and D_{HIGH}) in order to create a collision and overwash hazard map (Fig. 5).

The easternmost part (sector 1) has low R_{HIGH} values (Fig. 6). However, this segment is vulnerable to an overwash regime for storms with 5, 10 and 25 years of return period (Fig. 5). Both sectors 2 and 3 have similar calculated wave runup (Fig. 6). However, some areas found in sector 2 are vulnerable to events with 10 and 25 years of return period, whereas sector 3 is not represented as vulnerable to overwash (Fig. 5). Sector 4 is also not vulnerable, despite the intermediate R_{HIGH} elevation along the area (Fig. 6). From sectors 5 to 8 there is high urban development over the Ancão peninsula. Values for R_{HIGH} from sectors 5 to 7 are among the highest ones within the study area (Fig. 6). In this case, higher R_{HIGH} led to hazard-prone areas within these sectors for all defined storm scenarios (Fig. 5). Sector

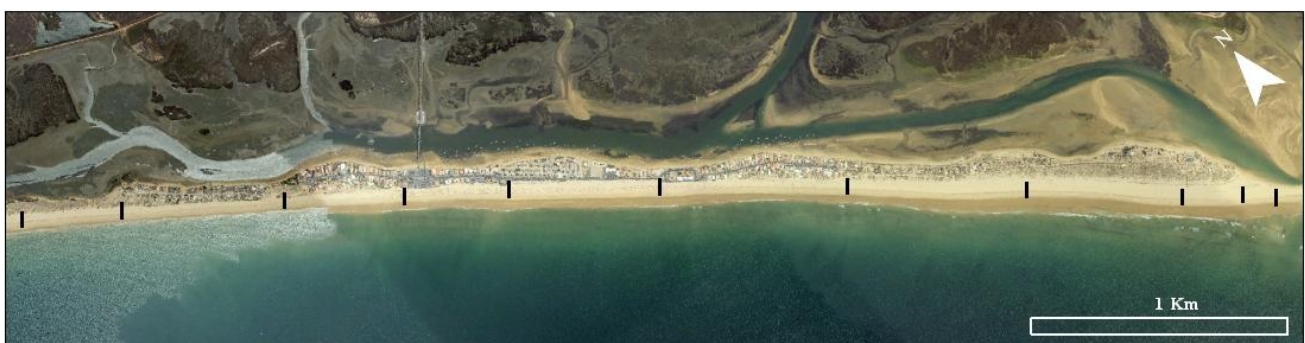


FIGURE 3 | Aerial photo of the study site and the ten individualised sectors.

TABLE 1 | Description of the sectors within the study area and the respective calculated beach slope

Sector	Characteristics	Beach Slope
1	Pristine area	0.072
	In accretion Dune height is 3.5 m (MSL)	
2	Sparse development in the backbarrier	0.064
	In accretion Dune height is 4.5 m (MSL)	
3	Sparse development in the backbarrier	0.061
	In accretion Most dissipative beach Dune height is 5 m (MSL)	
4	Development in the backbarrier Dune height 6.5 (MSL)	0.086
5	Intense development in the entire barrier width Dune is lowered or destroyed Dune height is 7 m (MSL)	0.123
6	Intense development in the entire barrier width Oceanfront with sand fences partially in-filled Top of wall's height is 6.0 m (MSL)	0.121
7	Intense development in the entire barrier width Most reflective beach Top of wall's height is 6.0 m (MSL)	0.124
8	Intense development in the entire barrier width Dune is lowered, occasionally covering a revetment Dune height is 6.5 m (MSL)	0.117
9	Development mainly in middle- to backbarrier Intense trampling on the foredune Dune height is 7.5 m (MSL)	0.123
10	Pristine area Dune ridge has blowouts and reach 8.5 m (MSL)	0.124

8 was classified under low overwash vulnerability caused by 10- and 25-year return period storms. High predicted R_{HIGH} were obtained for sectors 9 and 10 (Fig. 6), although the area is not equally vulnerable. The former had a few areas which could be overwashed during storms with 5, 10 and 25 years of return period. Sector 10 has high R_{HIGH} level, but it is not prone to overwash processes in any of the determined storm conditions (Fig. 5).

The surveyed dune base along the study area is entirely under collision regime for storms with 25 years of return period (Fig. 5). The representation of a collision regime caused by 5- and 10-year return period storms is mostly continuous.

DISCUSSION OF THE STUDY CASE

Overwash regime

The easternmost part of the study area (sector 1) is a dynamic zone driven by inlet processes. Tidal inlets are

one of the most dynamic parts of Ria Formosa barrier islands, therefore inducing extreme hazards of erosion and overwash (Vila-Concejo *et al.*, 2006). According to Matias *et al.* (2008) the Ria Formosa's most frequent washover formation mechanism between 1947 and 2001 was inlet dynamics, especially at the updrift areas, which produced 57% of inlet associated washovers (Matias *et al.*, 2008). Because the low-lying margin is under recent inlet updrift accumulation (Pacheco *et al.*, 2007), it is under an embryonic state of dune development which leads to high overwash vulnerability. The area has a low threshold and overwash occurs even during typical winter conditions.

The profile in Sector 2 is less vulnerable to an overwash regime because the beach face becomes wider, higher and the dune is more vegetated in relation to sector 1. In addition to natural processes controlling this sector, influence of human features can also be observed. There is an elevated coastal path that extends alongshore and across the dune ridge giving passage to beach users. This coastal asset ends over the foredune being therefore responsible for foredune and embryonic dune trampling, dune vegetation destruction, and promotes aeolian erosion. Consequently, artificial morphologies prone to overwash occur (Matias *et al.*, 2008).

Westward (sectors 3 and 4), the barrier island develops a wider beach and the foredune can reach from 5 to 8m above mean sea level. Apart from the eastern vulnerable portion of sector 3, which is still under the influence of foredune trampling, sectors 3 and 4 would not be affected by overwash events. The accretion leads to a wider beach, where there is berm development and dune enlargement. These areas are still under the influence of the updrift accumulation induced by the Ancão inlet. The inlet acts as a sediment trap because of tidal currents through the inlet channel, causing a seaward shoreline displacement along the updrift zone. Intermediate morphodynamic conditions were recorded along sectors 2, 3 and 4. These less reflective shores have more energy dissipation and, consequently, wave setup decreases (Benavente *et al.*, 2006). Hence, calculated R_2 , that includes wave setup, is reduced and leads to a lower R_{HIGH} . Lower R_{HIGH} levels induce lower overwash potential and shorter landward penetration.

The central area of Ancão peninsula (sectors 5 to 9) has a reflective beach face, high R_{HIGH} elevation and dense urban occupation. According to the results, from sector 5 to the eastern area of sector 9 the beach crest can be overwashed during storms with 5, 10 and 25 years of return period. The vulnerability of this area to extreme events is seen in Figure 7 where a storm with characteristics of a 5-year return period event strikes sector 7. Vulnerability to low storm intensity is often perceived in punctual areas, *e.g.* beach accesses. The steeper profile throughout the area has a corresponding effect on

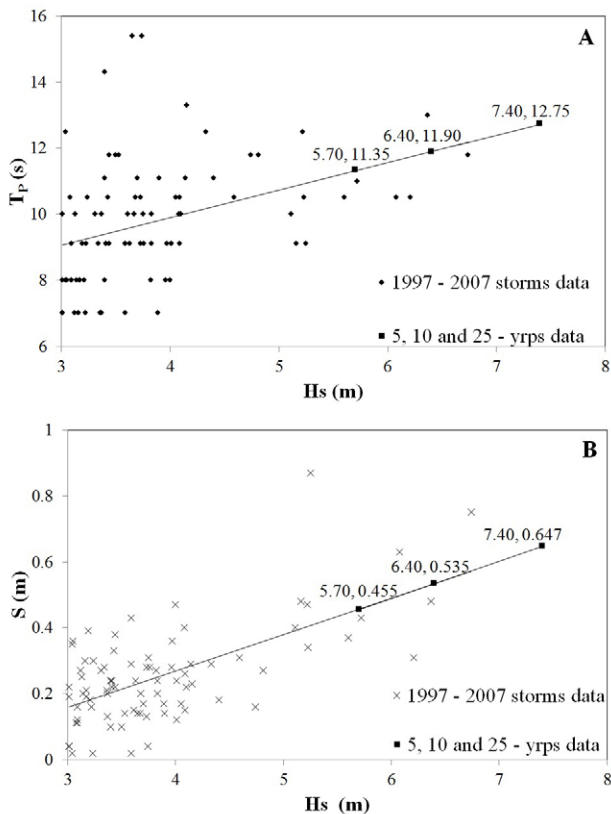


FIGURE 4 | Linear estimative of peak period (T_p) and storm surge (S) for the 5, 10 and 25-year return period storm. A) Daily highest wave significant height (H_s) versus peak period (T_p) from June 1997 to June 2007. B) Daily highest wave significant height (H_s) versus daily highest storm surge (S) from June 1997 to June 2007.

calculated runup elevations. Under surging wave conditions there is little dissipation of wave energy across the beach face, and the majority of wave energy is reflected on the slope, as observed by Stockdon *et al.* (2006) for other coastal areas with intermediate to reflective characteristics. Additionally, this coastal stretch congregates the most densely occupied area along the Ria Formosa (Praia de Faro). Along the coastline, human intervention is predominantly identified as shorefront buildings, foredune trampling and lowered or destroyed dunes. When present, the foredune is straighter if compared with what would occur under natural aeolian transport/construction as a result of aiding bulldozing, dune fences and revetments (particularly along sector 8). Man-made shore changes at this site altered the sediment budget and the coastal processes. The presence of coastal infrastructures avoids new embryo dune development and foredune restoration (Davidson-Arnott and Fisher, 1992), which increases the vulnerability to overwash (Andrade, 1990; Andrade *et al.*, 1998; Garcia, 2008).

Along the westernmost section of the study area the beach is narrow, steep and the estimated R_{HIGH} elevation is high. Some development is present in the eastern parts but within the last sector there is minimum or absent human

intervention. From the western area of sector 9 to sector 10 the dune ridge reaches up to 10m height above mean sea level and it evidences several aeolian erosional discontinuities in the form of blowouts on the top of the dune. Seaward, embryonic dunes have recently been formed. This accretion morphology is a consequence of updrift beach nourishments (undertaken since 1998; Oliveira *et al.*, 2008), which re-established a sedimentary source to the area. Despite the reflective beach slope, high runup elevation and erosional features within the dune ridge, there is low or null susceptibility to overwash, as also detected by Andrade (1990) and Andrade *et al.* (1998).

Collision regime

The dune base along Ancão peninsula is dominated by a collision regime. As a pre-overwash phase, the collision regime is associated with rising water levels, which leads to a reduction in overall beach width and consequently increases the potential to extensive damage to dune ridge in the form of dune scarping. If the identified coastal areas prone to collision do not store sufficient volume of sediment in the embryo dune zone and in the foredune, overwash will potentially occur (Davidson-Arnott and Fisher, 1992).

Along sector 1, dune base has low elevation reaching less than 3m above mean sea level. It is a low-lying zone where the dune ridge is recent and low and its base can be reached by low intensity storms. From sectors 2 to 4 the dune base reaches an average of 3.5m above mean sea level. Its seaward position, as a result of the wide dune ridge and recent accumulation, makes it more vulnerable to a collision regime. The distance of the dune from the shoreline is an important factor controlling its survival because of dissipation of wave energy within the beach face (Claudino-Sales *et al.*, 2008). Sector 5 is the single segment where a consistent dune area is not scarped by storms with 5 and 10 years of return period. There, the dune base has the highest elevation within the study area (5m above mean sea level). This elevation is noticeable even where the dune front was extensively substituted by buildings. The explanation for the high dune base elevation might be related to the existing shorefront restitution by placing sediments with bulldozers. The dune toe within sectors 6 and 7 often coincides with the base of constructions. This line is low, reaching 4m (mean sea level), and is largely under collision risk. The high vulnerability to collision regime under storms with short return periods is a consequence of the low dune base, its high exposition because of seaward location and reflective beach morphology.

From sectors 8 to 10 the dune base is the lowest registered within the surveyed area. The dune toe elevation is, on average, 2.2m (mean sea level) and it has a seaward advanced position. Besides the low-lying seaward dune base,

TABLE 2 | Significant wave height (H_s) determined by Pires (1998), and estimated wave peak period (T_p) and storm surge (S) for an event with different return period

Return Period (years)	H_s (m)	T_p (s)	S (m)
5	5.7	11.4	0.46
10	6.4	11.9	0.54
25	7.4	12.8	0.65

the reflective beach slope and high values of R_{HIGH} make the area extensively prone to escarpment.

DISCUSSION OF THE DEVELOPED METHODOLOGY

Method evaluation

Any hazard assessment involves a degree of uncertainty and this study is no exception. There is some inaccuracy in the methods used for field measurements and for over-

wash and collision hazards. These uncertainties are mostly related to the topographic survey (equipment and operator) and runup parameterisation. Differential GPS errors are related to satellite constellation and atmospheric conditions, and operator-induced errors include loss of antenna’s verticality and subjectivity in morphology edge interpretation (dune base and dune crest positioning). The expected errors in both the altimetric and planimetric point position can be, respectively, in a centimetric and decimetric scale.

R_{HIGH} calculation is an empirical parameterisation of the setup, swash and runup set for natural beaches. The highest calculated runup (R_{HIGH}) was occasionally underestimated since overwash was not predicted for all areas along the Ancão peninsula where overwash has been observed in the last decade. There are areas along the urbanised zone of Praia de Faro, especially within sectors 5, 6 and 7 where overwash occurs during storms with shorter return periods. These central areas of the peninsula are intensely urbanised which interferes with beach morphology, including beach width reduction and increased steepness due to rigid prom-

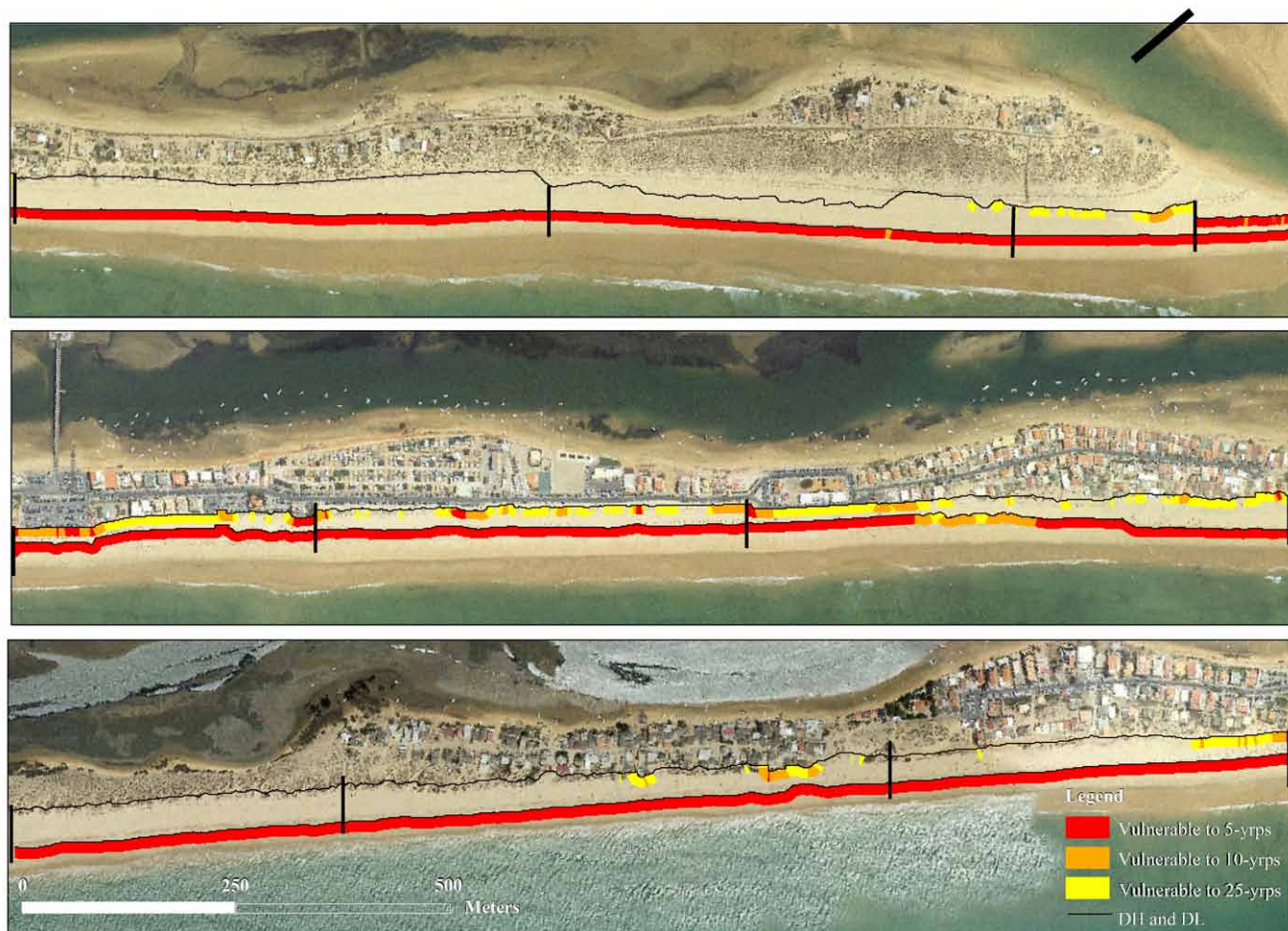


FIGURE 5 | Representation of collision and overwash regimes vulnerability along the study area for 5, 10 and 25-year return period storms. D_H represents the dune crest position whereas D_L is dune base, which is downward from the georeferenced site for better map representation.

inent structures at the upper beach. The predictive model of Stockdon *et al.* (2006) is dependent on the foreshore beach slope, *i.e.* alongshore-variable slopes imply similar alongshore variability in swash excursion and runup elevation. Stockdon *et al.* (2006) compared a relative slope difference to a relative runup error when alongshore-averaged slope is used instead of a more accurate slope measure at each alongshore line. On intermediate and reflective beaches with complex foreshore topography, the alongshore variability in beach steepness may result in a relative runup error equal to 51% of the variability between the measured and the mean slope. Additionally, the mean difference between estimated and measured runup for the research performed by Stockdon *et al.* (2006) was about -18cm, indicating that the parameterisation tends to slightly underestimate the elevation of runup.

In relation to the collision regime, the presence of the berm is an important controlling factor because the berm width can restrain the process. Wide berms tend to reduce the limit of the overtopping runup (Horn and Ling, 2006) hence, runup may reach the predicted D_{LOW} height, but cannot attain the dune toe and collision regime is not achieved. Variations in berm width can be seen along the study area, *e.g.* from sectors 2 to 4 the berm is wide, but narrows at sectors 9 and 10. As beach face slope calculation assumes a linear profile, runup computations cannot effectively adjust to beach morphodynamic differences caused by berm variability, and therefore collision regime does not completely reproduce field observations.

An important aspect of the applied method is the seasonal and annual dataset variation. Frequency and intensity of storm surges and W-SW energetic waves are strongly variable during the year as a response of the storm events distribution throughout the seasons. Beach morphology at

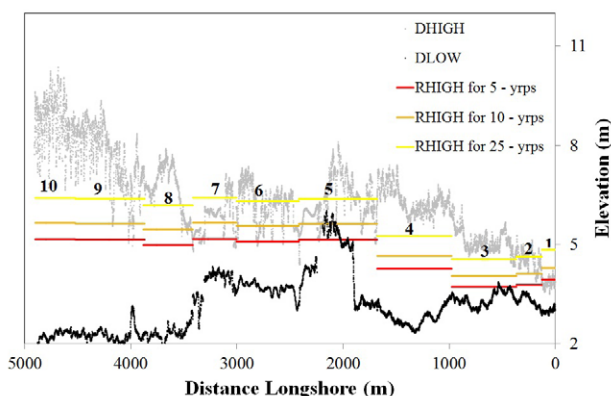


FIGURE 6 | Alongshore profile of dune crest (D_{HIGH}) and dune base (D_{LOW}) heights above mean sea level and the calculated runup (R_{HIGH}) for different storms scenarios and for the ten sectors established along the Ancão peninsula.

the time of survey is dependent on a number of factors such as beach seasonality, its response to the latest energetic events, beach recovery rates and sediment budget of the littoral cell. Hence the beach slope, which is a controlling factor for both overwash and collision regimes, will cause different scenarios depending on the time of year that the beach survey was undertaken.

In this study, for the computation of the key parameter R_{HIGH} , average mean high water was considered, which yields important consequences in results. Storms with identical characteristics that act over lower or higher tidal levels will respectively induce lower or higher overwash vulnerability. According to Hofstede (1997) in a tidal coastal environment, the water level normally remains for much longer periods around the mean high water than around mean sea level. Moreover, all storms with more than 5 years of return period will last more than 2 days and eventually will act over a high tide level.

A high coincidence was noticed between obtained results and overwash areas observed in last 15 years. The depicted areas in the map (Fig. 5) where collision and overwash are likely to occur correspond to regions along Ancão peninsula where there are records of overwash and erosion caused by high wave energy events. This correspondence between the predictive method and observed occurrences confers applicability to the current approach for overwash hazard assessment.

Management application

Storms are important factors defining shoreline position and erosion history along a coastline. The identification of vulnerable coasts enables coastal mapping which is a tool for coastal management and decision making. Return period is a significant concept in this perspective and setting: storm impacts with a short return period are significant because they determine the likeliness of occurrence of events. By understanding the magnitude and return period of storms it is possible to provide more accurate and comprehensive information to help coastal managers in emergency planning and impact reduction of natural disasters. Overwash, with subsequent landward transport of water and sediment may cause damage or loss of properties, and ultimately lead to coastal inundation that frequently causes injury or loss of human lives.

The Ancão peninsula is the western limit of the Ria Formosa natural park, which was created in December, 9th 1987. Besides, the coastal protected area is also designated as a wetland of international recognition (Ramsar, 2008). The Ria Formosa natural park land use management plan (POP NRF), produced in 2001, considers the Ancão peninsula as “mostly highly” vulnerable to overwash and “high-



FIGURE 7 | Examples of overwash at Praia de Faro parking place (sector 7) during the 2th March 2010 storm, with conditions similar to a 5 year return return period storm.

ly” vulnerable to barrier breaching. The obtained results corroborate this classification on a scientific basis. Nevertheless, they allow a better detail and remark the areas within the Ancão peninsula which are prone to overwash and collision at a given time-scale (return period) and those expected to be safer. A management approach for the Ancão peninsula should consider these differences as well as their economic implications. Conflicts are expected considering the broad range of interests and stakeholders (traders, fishermen, beach users, tourists) and the condition of natural park. These conflicts rely especially on economic interests and conservation aspects. The increased human pressure in the system, especially along Praia de Faro, has been causing dune destruction or intense dune trampling that promotes the development of fragile sites. During high energy wave events, overwash occurs within these lowered gaps. This proves that most of the overwash areas have a human intervention causal component (Matias *et al.*, 2008). Overwash acts as a trigger mechanism for other hazards, such as barrier breaching and subsequent new in-

let installation, which can impact the economical value of the region in a drastic way.

In order to obtain a final management plan for the area, mapping of vulnerable areas must be carried out and protective actions must be taken. Mapping of exposed areas is strongly recommended, particularly for shorelines evolving in response to natural processes and human activities. Hence, overwash vulnerability may be seen as a local strategy for protection and relocation of coastal communities, alteration of future urban development, emergency planning and for flooding assessments.

CONCLUSIONS

Setting the correct ocean’s forcing is crucial when analysing potential areas to overwash processes. Wave attributes (significant wave height and wave length), and astronomical and meteorological tides are key factors driving overwash occurrence. By choosing the best method for calculation of runup vertical scaling and tides elevation, and matching it to dunes elevation, the overwash potential is well defined. Storm impacts are not equally identified along a barrier island due to the combined effects of along-shore-variable morphology of the beach and dune relative to the intensity of the ocean’s forcing.

For the study case of Ancão peninsula, collision regime is shown as a constant hazard, whereas overwash hazard varies temporally and spatially alongshore. The shore is largely affected by a storm with 25 years return period, whereas a storm with 5 years return period promotes overwash only at particular sites. For eastward immature and low dune crests, there is a significant connection between the overwash vulnerability and tidal inlet presence. The central area is the most vulnerable to overwash not only because of the reflective beach slope but also due to the lowering and destruction of dunes by human intervention. Ancão peninsula has physiographic characteristics prone to overwash, such as the narrow barrier, the reflective beach slope and the exposition to the energetic SW events. However, the presence of a high dune ridge westward provides low vulnerability to overwash. These results highlight the importance of preserved dunes as a natural shoreline protection against storm overwash.

The quantification of runup levels and coastal morphology for the establishment of hazard maps provide more objective identification of areas prone to overwash when compared to methods applied in previous studies for Ancão peninsula. Moreover, hazard maps are effective tools for coastal management and planning. The developed method proved to be effective on the assessment of overwash vulnerability and can therefore be widely used on similar

coastlines. The method's results can be applied to set building standards, land use guidelines along the coast and provide information for evaluation and design of coastal intervention (such as fencing, nourishment and inlet relocation or stabilisation).

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